



Effects of Volumetric and Mechanistic Test Variability on Predicted Performance of Asphalt Pavements Using the MEPDG

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- Transition from empirical design to mechanistic-empirical design procedures
 - Requires material inputs
 - Evaluate the effect of the variability of inputs on predicted performance
 - Establish confidence in performance predictions
- Deviation from either material or construction specifications often lead to premature pavement distresses or even failure

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- MEPDG features the prediction of pavement performance
 - Rutting
 - Cracking
 - Smoothness
- The design guide software
 - Four Modules
 - Project Summary,
 - Traffic,
 - Environmental/Climate, and
 - Pavement Structure
 - Material Characterization

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- MEPDG: Material input module
 - Based on hierarchal structure
 - Level 1 - measured mechanistic properties
 - Level 2 - predicted mechanistic values
 - Level 3 - national default values
 - Volumetric/Mechanistic
 - Laboratory testing
 - Variability

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- Adequate QA practices
 - Ensure HMA properties conform to specifications
 - Avoid premature failure of HMA
- How does the variability effect predicted pavement performance?
- The NCHRP Project 9-48, “Field versus Laboratory Volumetrics and Mechanical Properties,”
 - initiated to quantify sources and causes of variability in the measurements of volumetric and mechanical properties of dense-graded asphalt mixtures

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- Evaluate the effects of variability of volumetric and mechanistic properties on predicted performance
 - asphalt pavements using the MEPDG.

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- Collected volumetric and mechanistic properties
 - Survey
 - 13 state DOTs and FHWA Trailer
 - To quantify variability



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- Volumetric Properties
 - Asphalt Content
 - Air Voids, VMA, VFA
 - Gmb, Gmm
 - Field Density
- Mechanistic Properties
 - Dynamic Modulus, Phase angle
 - Flow Number
 - Indirect Tensile Strength
- Three Pavement Structures
 - Low Traffic
 - Medium Traffic
 - High Traffic

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- Effect of volumetric variability on predicted mechanistic properties of asphalt mixtures using the
 - Fonseca-Witczak predictive model was quantified
 - Monte Carlo simulation.
- Effects of mechanistic variability on the design outcomes were evaluated using the MEPDG.

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Quantification of Variability in HMA Design Inputs

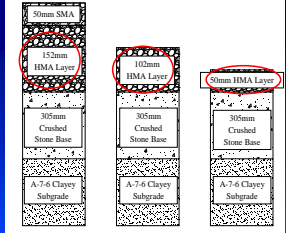
- Two main types of statistical analyses were conducted in order to quantify the magnitude of the variability of volumetric and mechanistic properties:
 - statistical analysis of the individual data sets
 - From the 13 DOTs and FHWA
 - a meta-analysis of the combined data sets
 - national average of variability
- Interim Report
 - NCHRP Project 9-48

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Pavement Performance Prediction

- The MEPDG software was used to predict the performance of three typical Louisiana pavement structures for three traffic levels
 - Low
 - Medium
 - High
- Varying HMA Layer



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MEPDG Design Inputs

- New flexible pavement
 - service life of 20 years
- Pavement failure limits
 - LADOTD criteria

| Distress | Traffic Level (AADTT) | | |
|----------------|-----------------------|-------------------|-------------------|
| | High (14,554) | Medium (1,992) | Low (816) |
| IRI (mm/km) | 1973 (125in/mile) | 3175 (200in/mile) | 3969 (250in/mile) |
| Rut Depth (mm) | 9.6 (3/8in) | 14.2 (9/16in) | 14.2 (9/16in) |

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MEPDG Traffic Inputs

- LADOTD provided values for multiple traffic classifications
 - average annual daily traffic (AADT),
 - truck factors, and
 - vehicle class distribution
- Default values developed from LTPP data for hourly distribution and growth factor were used.

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Climate

- Climatic data were obtained from the MEPDG climate database for the city of Baton Rouge, Louisiana
- The water table depth (2.1m) was calculated via the relationship based on surface elevations in the Gulf Coast regions in the United States (14)

$$\text{Water Table Altitude} = \text{Land-surface altitude} * 0.8978$$

- The land-surface elevation was determined from the MEPDG climatic database


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HMA Dynamic Modulus

- Variation of predictive E* based on variability of material input
 - Variability based on 13 state DOTs data
 - Monte Carlo simulation

$$E^* = \frac{3.071977 - 0.0024 \rho_c - 0.00085 \rho_{agg} - 0.000017 (p_{agg})^2 + 0.005407 p_{agg}}{2.4 * (-0.683313 - 0.343357 \ln(V_v) - 0.383328 \ln(V_v))}$$

- Input:
 - Binder Viscosity
 - Binder Content
 - Air Voids
 - Gradation
- Laboratory measured
 - AASHTO TP 79
 - FHWA
 - University of Arkansas
 - MnRoad



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Base and Subgrade Properties

- Resilient Modulus values for crushed limestone base and clayey subgrade were collected determined from literature (15)
- These values were kept constant for each pavement structure.

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Individual States Analyses

- Collect Data
 - 13 States and FHWA Trailer provided data sets.
- Each data set: Determine variability
 - volumetric and mechanistic properties
 - Standard deviation and coefficient of variation
- “National Average Variability”
 - computed
- Example - Oklahoma DOT
 - OK site manager
 - Volumetric and Gradation data: 2,163 Mixtures
 - Air Void,
 - Voids in the Mineral Aggregate,
 - Mixture Bulk Specific Gravity (Gmb),
 - Asphalt Content, and
 - Aggregate Gradation

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Oklahoma DOT Analysis

- Levels of Variability in Oklahoma DOT Volumetric Properties

| Property | Variability (St. Dev.) | CV (%) | Number of Mixtures |
|----------------------------|------------------------|--------|--------------------|
| Air Voids (SSD), % | 0.38 | 10.3 | 2001 |
| Asphalt Content, % | 0.20 | 4.4 | 935 |
| VMA, % | 0.38 | 2.9 | 1796 |
| G _{mb} | 0.008 | 0.3 | 2004 |
| Passing 19.0 mm (3/4") | 1.75 | 1.6 | 322 |
| Passing 12.5 mm (1/2") | 2.04 | 2.3 | 831 |
| Passing 9.5 mm (3/8") | 2.43 | 3 | 1001 |
| Passing 4.75 mm (No. 4) | 2.72 | 4.6 | 1002 |
| Passing 2.36 mm (No. 8) | 2.17 | 5.3 | 1002 |
| Passing 1.18 mm (No. 16) | 1.7 | 5.7 | 1002 |
| Passing 0.6 mm (No. 30) | 1.43 | 6.2 | 1002 |
| Passing 0.3 mm (No. 50) | 1.18 | 7.4 | 1002 |
| Passing 0.15 mm (No. 100) | 0.83 | 9.2 | 1002 |
| Passing 0.075 mm (No. 200) | 0.49 | 9.6 | 1002 |

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Average Variability of Volumetric Properties

- Average of Volumetric Variability Determined from 13 states data sets

| Property | Sample Type | Range of St. Dev. | Average St. Dev. |
|--------------------|-------------|-------------------|------------------|
| Asphalt Content, % | PL | 0.17 – 0.24 | 0.21 |
| Air Voids, % | PL | 0.36 – 0.99 | 0.62 |
| VMA, % | PL | 0.37 – 0.65 | 0.54 |
| VFA, % | PL | 3.40 – 5.16 | 4.28 |
| G _{mb} | PL | 0.008 – 0.018 | 0.013 |
| G _{mb} | PF | 0.016 – 0.025 | 0.021 |
| G _{mm} | PL | 0.005 – 0.012 | 0.009 |
| Field Density, % | PF | 0.74 – 1.49 | 1.12 |

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Average Variability of Volumetric Properties

- Average of Aggregate Gradation Variability Determined from 13 states data sets

| Sieve Size | Sample Type | Range of St. Dev. | Average St. Dev. |
|--------------------|-------------|-------------------|------------------|
| 25.0 mm (1") | PL | 0.68 – 2.66 | 1.67 |
| 19.0 mm (3/4") | PL | 0.82 – 2.59 | 1.71 |
| 12.5 mm (1/2") | PL | 0.89 – 3.54 | 2.22 |
| 9.5 mm (3/8") | PL | 1.61 – 3.75 | 2.68 |
| 4.75 mm (No. 4) | PL | 1.87 – 3.48 | 2.68 |
| 2.36 mm (No. 8) | PL | 1.75 – 2.73 | 2.24 |
| 1.18 mm (No. 16) | PL | 1.56 – 2.05 | 1.81 |
| 0.600 mm (No. 30) | PL | 1.37 – 1.89 | 1.63 |
| 0.300 mm (No. 50) | PL | 1.07 – 1.28 | 1.18 |
| 0.150 mm (No. 100) | PL | 0.64 – 0.99 | 0.82 |
| 0.075 mm (No. 200) | PL | 0.34 – 0.84 | 0.59 |

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Average Variability of Mechanistic Properties

- Average of Mechanistic Variability Determined from 13 states data sets and FHWA Trailer


| Properties | CV (%) Range | | Average CV (%) | Number of Mixtures |
|---------------------------|--------------|------|----------------|--------------------|
| | Min | Max | | |
| Dynamic Modulus | 10.0 | 23.8 | 13.9 | 58 |
| Phase angle | 3.9 | 15.4 | 7.1 | 58 |
| Flow Number | 37.3 | 52.1 | 45.2 | 89 |
| Indirect Tensile Strength | 11.9 | 15.4 | 13.7 | 9 |

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Variability of Dynamic Modulus

- %CV = 13.9%
 - Measured from laboratory tests
 - FHWA
 - State of Arkansas
 - Midroad
- %CV = 8.1%,
 - Based on Monte Carlo simulation of 10,000 repetitions
 - 13 DOTs



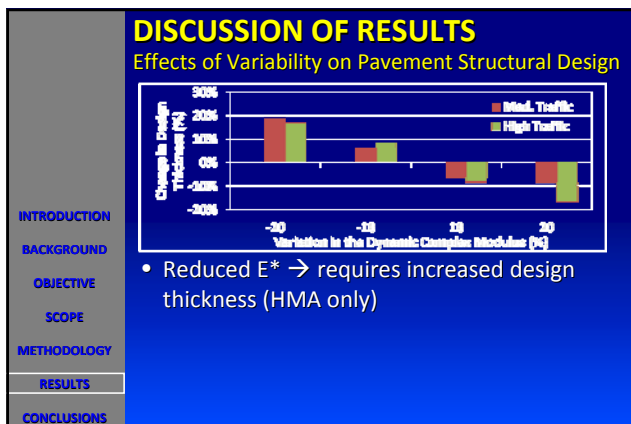
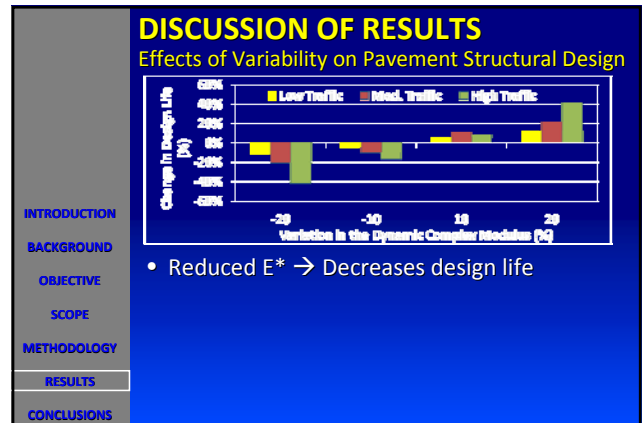
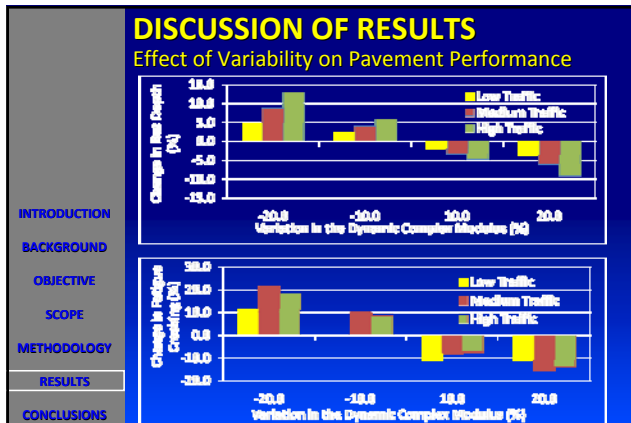
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Effect of Variability on Predicted Pavement Performance

- MEPDG Software was used
- Three levels of Dynamic Modulus
 - Mean, Mean ± 10%, Mean ± 20%
- Measured effects of predicted pavement distresses
 - Rutting
 - Fatigue Cracking
 - Smoothness

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SUMMARY and CONCLUSIONS

- Variation of E^* was determined
 - Predictive equation
 - Laboratory test results
- Average CV in E^* was 8.1%
 - calculated from the Fonseca-Witczak model
- Average CV in E^* was 13.9%
 - Laboratory test data
- Variability in volumetric properties will not affect the accuracy of the design when
 - Level 2
 - Fonseca-Witczak Model

CONCLUSIONS

- Predicted pavement distresses from MEPDG indicated
 - Variability level in the $E^* \leq 10\%$ → predicted level of performance of $\leq 10\%$
 - Variability level in the E^* up to 20% → design life of the pavement structures by up to 42%
 - Variability level in the E^* up to 20% → design HMA thickness up to 19%.
- Predicted top-down cracking damage over the pavement service life was minimal
 - predicted top-down cracking was not greatly influenced by the variability E^*

